

**University of Stuttgart**

Institute of Combustion and Power Plant Technology

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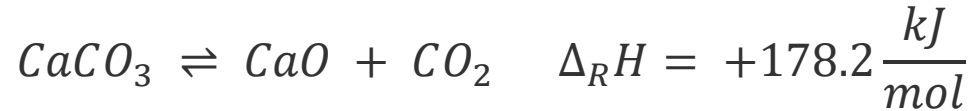
# Demonstration of Calcium Looping CO<sub>2</sub> capture for cement plants at semi industrial scale

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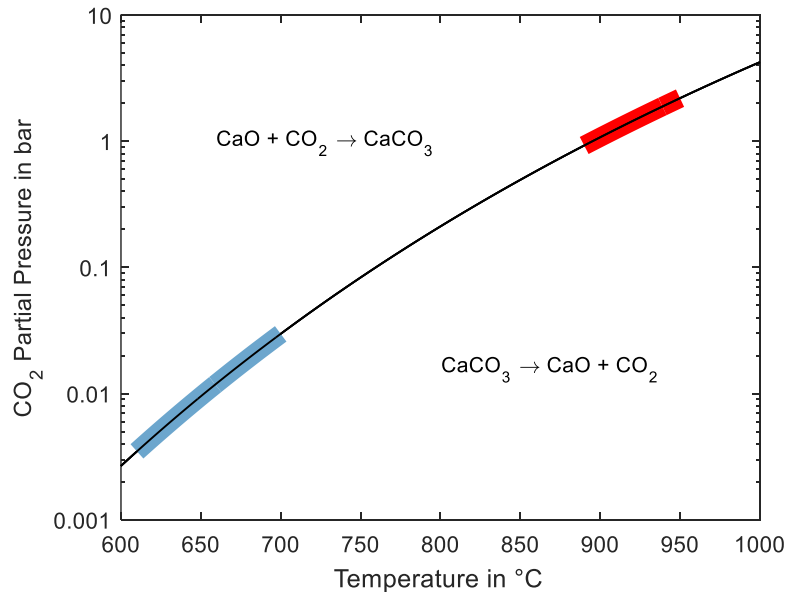
14<sup>th</sup> GHGT, 22<sup>nd</sup> October,  
Melbourne, Australia

**Fundamentals of  
Calcium Looping  
CO<sub>2</sub> capture from  
cement plants**

# Calcium Looping CO<sub>2</sub> capture

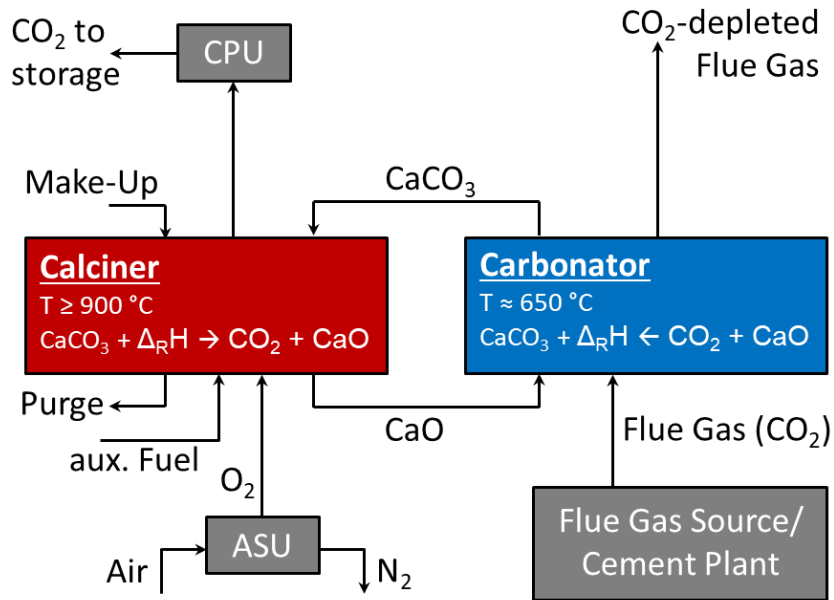
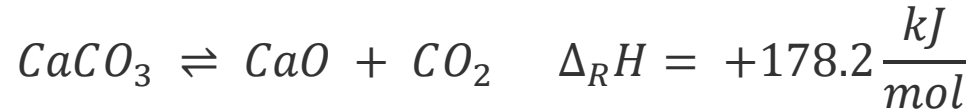


Calcination-carbonation equilibrium calculated by



- Solid sorbent cycle process
- CO<sub>2</sub> capture by cyclic calcination and carbonation of CaCO<sub>3</sub>/CaO
- Efficient energy recuperation because of high temperature level

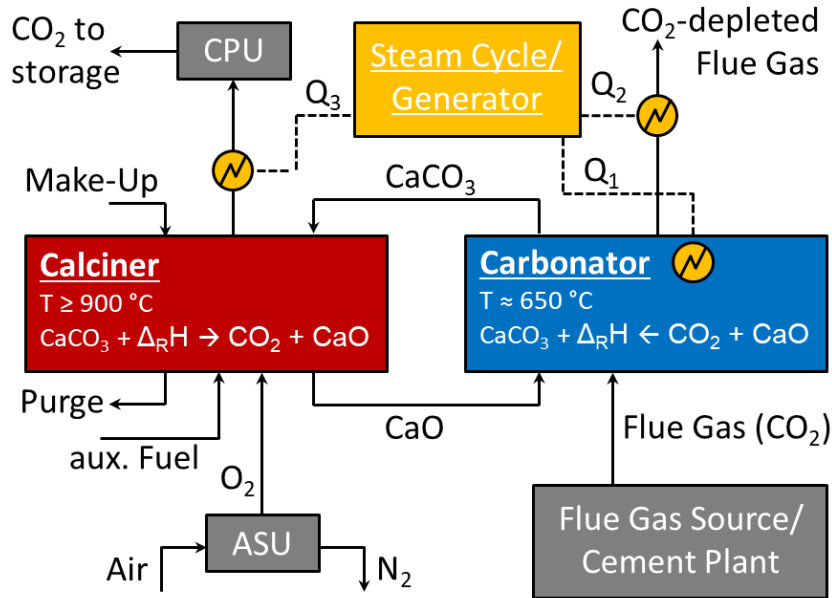
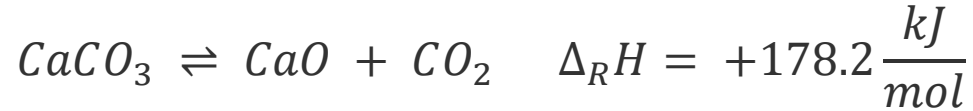
# Calcium Looping CO<sub>2</sub> capture process



## Definitions

- Sorbent activity:  $X_{avg} = \frac{M_{\text{CO}_2}}{M_{\text{Sorbent}}}$
- Make-Up ratio:  $\frac{\dot{N}_{\text{CaO}, \text{fresh}}}{\dot{N}_{\text{CO}_2, \text{Carb}, \text{in}}}$
- Looping ratio:  $\frac{\dot{N}_{\text{CaO}, \text{trans}}}{\dot{N}_{\text{CO}_2, \text{Carb}, \text{in}}}$

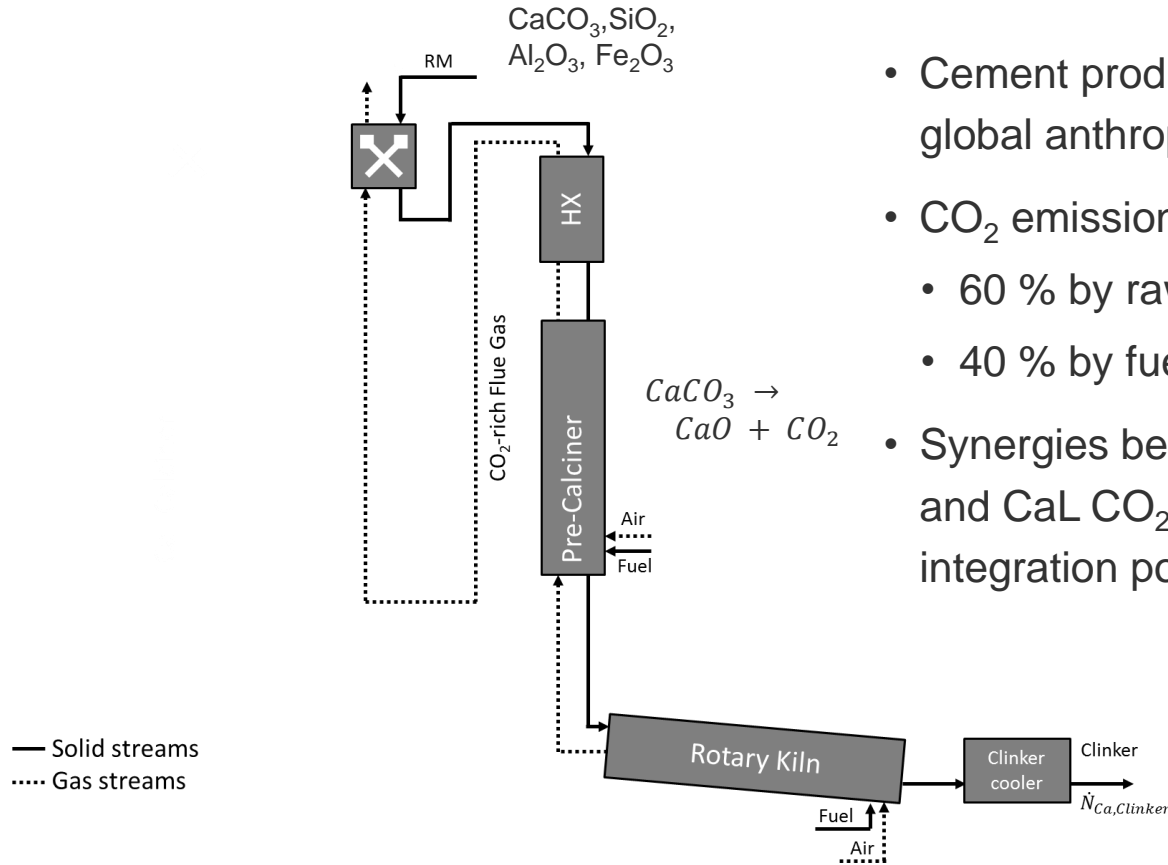
# Calcium Looping CO<sub>2</sub> capture process



## Definitions

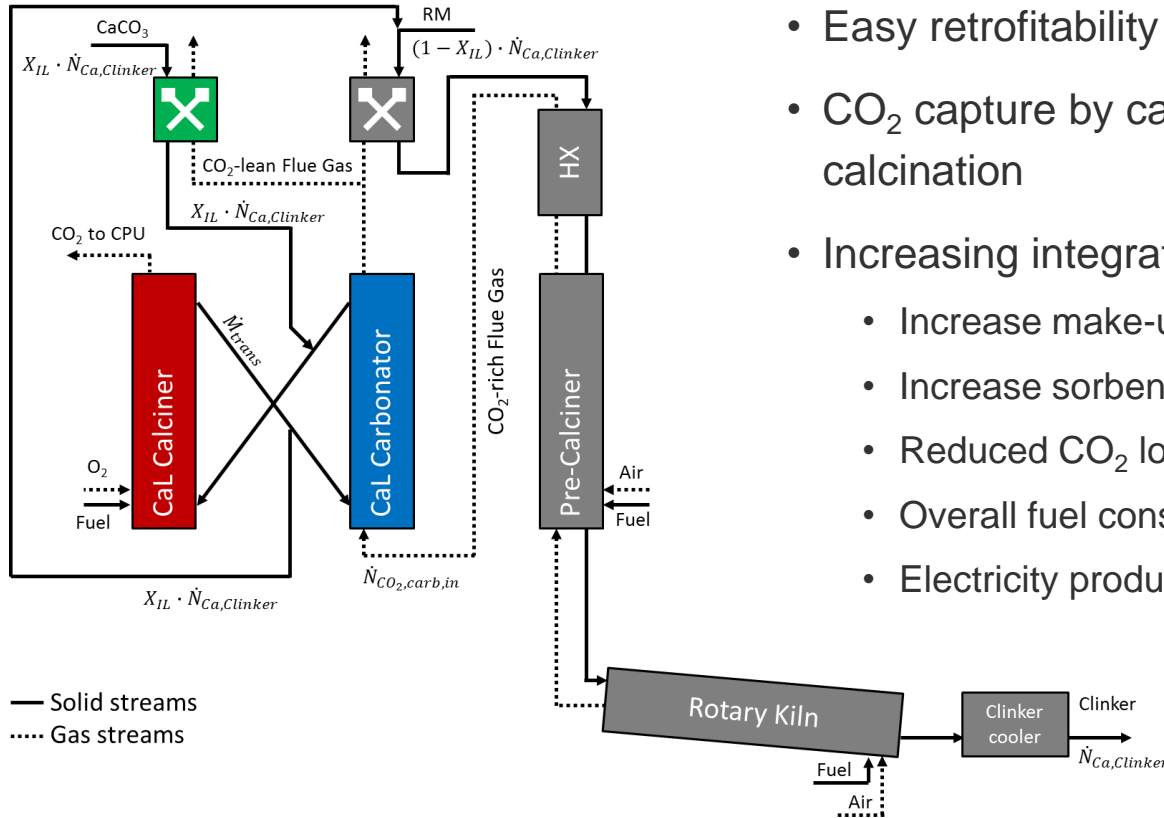
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# Clinker manufacturing process



- Cement production constitute ~5-8 % of global anthropogenic  $\text{CO}_2$  emissions
- $\text{CO}_2$  emissions:
  - 60 % by raw materials
  - 40 % by fuel
- Synergies between clinker manufacturing and CaL  $\text{CO}_2$  capture by solid and energy integration possible

# Tail-end Calcium Looping CO<sub>2</sub> capture from cement plants



- Easy retrofitability
- CO<sub>2</sub> capture by carbonation and oxy-fuel calcination
- Increasing integration level ( $X_{IL}$ ) leads to:
  - Increase make-up to CaL system
  - Increase sorbent activity
  - Reduced CO<sub>2</sub> load (CaL oxy-fuel calcination)
  - Overall fuel consumption increases
  - Electricity production (CO<sub>2</sub> neutral)

$$X_{IL} = \frac{\dot{N}_{CaO,CaL}}{\dot{N}_{CaO,Clinker}}$$

# **Methodology / experimental set-up**



# Fluidized Bed Research Facilities – MAGNUS

**200 – 230 kW<sub>th</sub> pilot scale facility (3 reactors)**

Bubbling bed reactor (1x)

- diameter: 330 mm
- height: 6 m

Circulating fluidized bed reactor (2x)

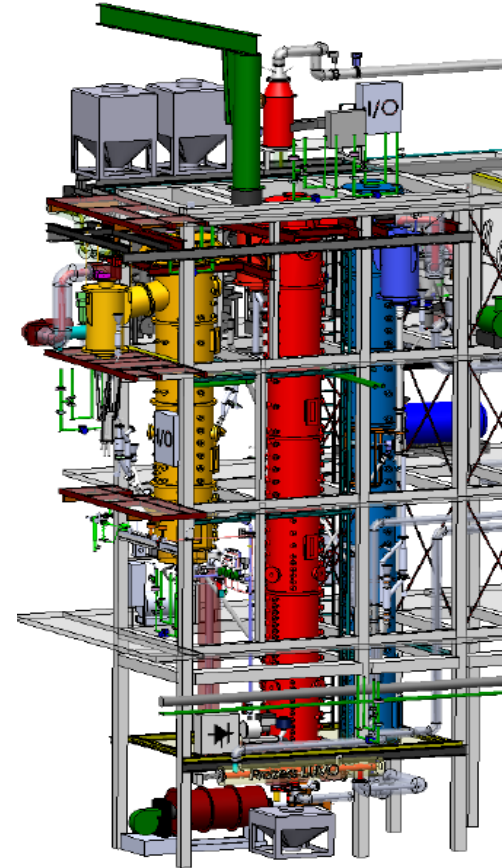
- diameter: 200 mm
- height: 10 m

Possible reactor configuration: CFB-CFB, BFB-CFB

Hot flue gas recirculation for oxy-fuel combustion

Gas analysis (CO<sub>2</sub>, O<sub>2</sub>, CO, SO<sub>2</sub>, NO<sub>x</sub>, CH<sub>4</sub>, H<sub>2</sub>, C<sub>x</sub>H<sub>y</sub>)

No electrical heating (heated by combustion)



# Experimental conditions

- CO<sub>2</sub> flue gas concentration: 15 – 33 vol%
- Volume Flow: up to 180 Nm<sub>3</sub>/h (~ 0.1 % of cement plant flue gas)
- Make-up flow/ratio: up to 50 kg/h / 1 mol<sub>CaO</sub>/mol<sub>CO<sub>2</sub></sub> ;

Limestone	CaO	MgO	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Others	CO <sub>2</sub>
	wt%, wf	wt%, wf	wt%, wf	wt%, wf	wt%, wf	wt%, wf
Western Germany	54.5	0.7	0.4	1.2	0.2	43.0

\*determined by TIC

Coal	C	H	O*	N	S	Ash	H <sub>2</sub> O	H <sub>i</sub>
	wt%, waf	wt%, waf	wt%, waf	wt%, waf	wt%, waf	wt%, wf	wt%, ad	MJ/kg, wf
Columbian I	80.3	4.9	12.3	1.9	0.6	9.6	7.4	28.98
Columbian II	77.6	5.3	14.4	1.6	1.1	9.13	7.4	28.09

\*calculated by difference

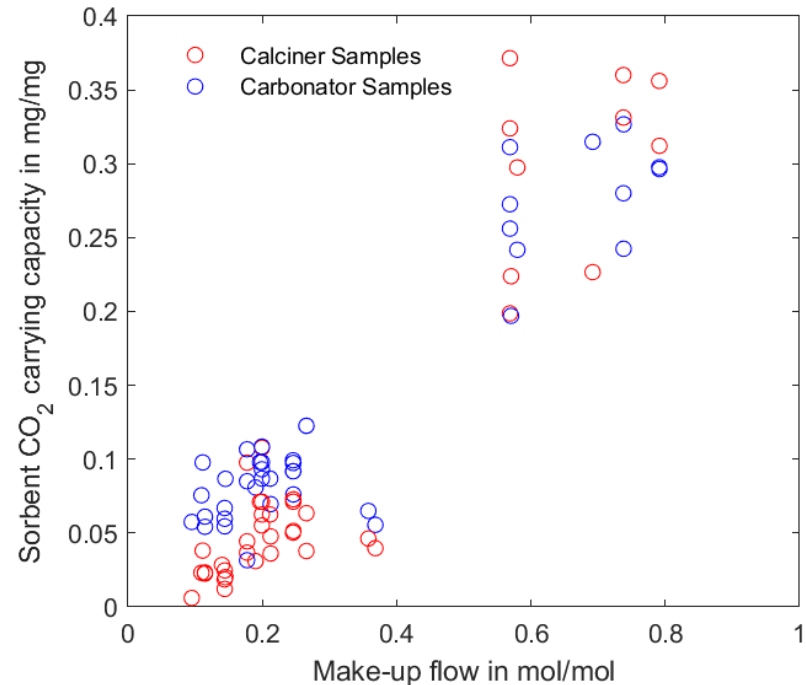
wf: water free;  
waf: water and ash free;  
ad: air dried

# **Results and discussion**

# Results and discussion – Sorbent CO<sub>2</sub> carrying

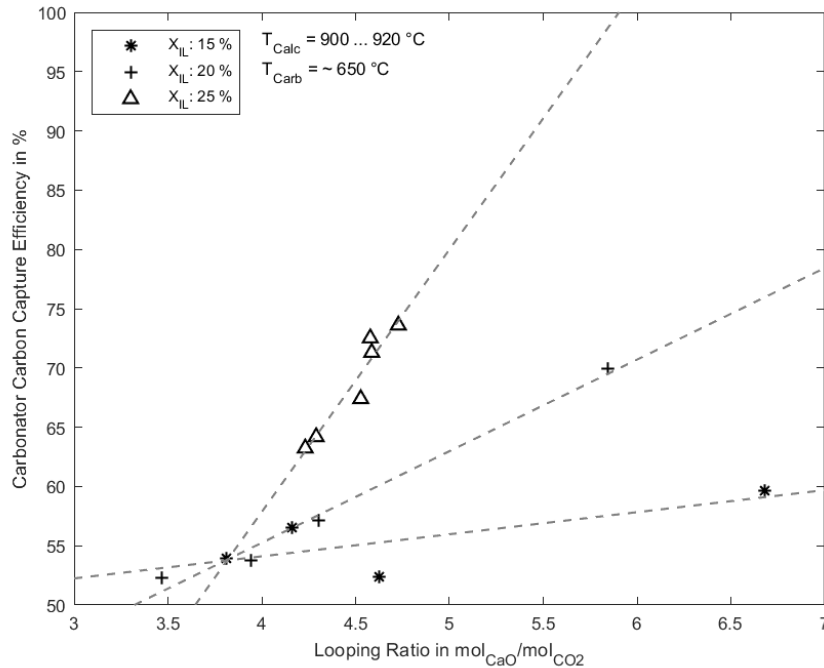
- Sorbent capacity depends strongly on make-up ratio (“sorbent age”)
- At lower make-up ratios sorbent activity of carbonator samples significantly higher than calciner samples
- Hydration during cooling of samples higher for carbonator samples  
→ indicates structural during carbonation

Average sorbent capacity of carbonator and calciner samples taken during the experimental campaigns



# Results and discussion – CO<sub>2</sub> capture performance

Carbonator CO<sub>2</sub> capture efficiency vs looping ratio at lower integration levels

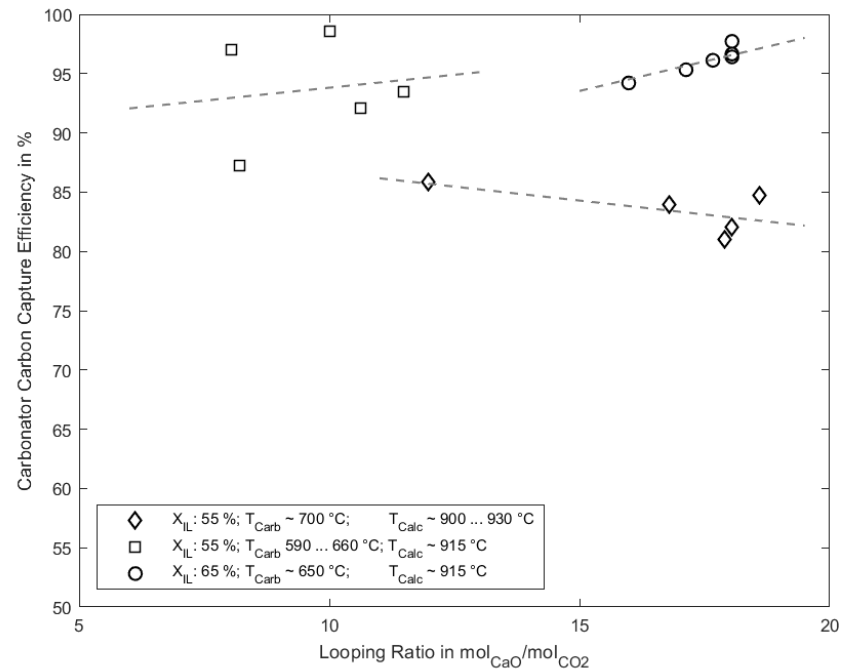


- Higher CO<sub>2</sub> concentration at lower integration levels leads to reduced looping ratios
  - Limitation of CO<sub>2</sub> capture by incoming amount of (active) CaO
- ➡ CO<sub>2</sub> capture increases with looping ratio
- ➡ Stronger improvement of CO<sub>2</sub> capture with looping ratio at higher integration level

# Results and discussion – CO<sub>2</sub> capture performance

- CO<sub>2</sub> capture up to 98 % achieved due to high sorbent activity
- Limitation of CO<sub>2</sub> capture by calcination-carbonation equilibrium at higher integration levels
- No influence on CO<sub>2</sub> capture efficiency at higher integration levels (i.e. make-up ratios)

Carbonator CO<sub>2</sub> capture efficiency vs looping ratio at enhanced integration levels



# Conclusion

# Conclusion

- Synergies between clinker manufacturing and Calcium Looping CO<sub>2</sub> capture due to use of common feedstock (CaCO<sub>3</sub>)
- Different integration levels (15 % to 65 %) for a tail-end Calcium Looping cement plant system has been assessed
- Calcium Looping CO<sub>2</sub> capture for cement application has been investigated at IKF's 200 kW<sub>th</sub> Calcium Looping pilot plant achieving CO<sub>2</sub> capture efficiencies up to 98 %
- Sorbent's CO<sub>2</sub> carrying capacity improves with increasing integration level (i.e. make-up)
- For lower integration levels a significant improvement of CO<sub>2</sub> capture with increasing looping ratio was found, while for higher integration levels the CO<sub>2</sub> capture was limited by the carbonation equilibrium



# Thank you for your attention!



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# Thank you!



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